DRAWINGS ATTACHED

(21) Application No. 53819/69 (22) Filed 3 Nov. 1969

(31) Convention Application No. 777 413 (32) Filed 20 Nov. 1968 in

(33) United States of America (US)

(45) Complete Specification published 25 Aug. 1971

(51) International Classification F 16 1 9/16

(52) Index at acceptance B8P 21B 4A 4K

F2P 1A11 1A24 1B3 1B6 1B7



(54) TUBULAR MEMBER

We, CLEVEPAK CORPORATION, a Corporation organised and existing under the laws of the State of Delaware, United States of America of 6201 Barberton 5 Avenue, Cleveland, Ohio 44102, United States of America, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be parti-10 cularly described in and by the following statement:-

With many containers, especially corrugated or solid fibre boxes, the side walls often require reinforcement so that the con-15 tainer can withstand certain stresses and strains. For example, when containers are stacked one upon another and the containers rather than the contents must provide the support, the walls of the lowermost con-20 tainers in a stack must bear substantial forces which tend to deform the side walls. If the walls are permitted to deform significantly, any fragile contents may suffer damage.

To increase rigidity, wooden corner posts. corrugated or fibrous posts or cylindrical tubes have been inserted in containers to provide reinforcement along particular coordinates. Wooden posts are becoming more 30 costly and interfere in conventional scrap carton recycling, wherein containers are shredded for return to paper makers. Corrugated and fibrous posts are often inadequate in strength, when large stresses are to 35 be placed upon containers in which they are the primary reinforcement. This is because the typical shaping cuts reduce their load-bearing capacity. Cylindrical tubes, besides occupying peripheral storage space, 40 contact containers only tangentially along the tube length and this minimal surfaceto-surface contact provides little abutment strength even when the tube is adhered to the container walls for reinforcing a con-

45 tainer in a direction transverse to the axis [Price 25p]

of such tubes.

In accordance with the invention, an elongate stiff tubular supporting member has a unitary wall including at least one layer of material extending jointlessly around its 50 whole periphery, the wall being substantially triangular in cross section and incorporating elongate strength-giving components aligned predominately longitudinally of the mem-

Such members may be used in many applications for example as short vertical legs of a carton, or as horizontal skids for a pallet. Their prime use, however, is as reinforcing supports or columns for the walls 60 of corrugated or other containers and, when stuck into the corners of rectangular boxlike containers, they integrate with the container walls to provide both axial and transverse strength against carton deformation. 65 The construction is essentially jointless, strong and lightweight, and has planar or slightly curved sides forming a triangular or substantially triangular shape, so that the sides provide a large contact area for bear- 70 ing against and securing to the walls of the container. Such tubular constructions may be inserted singly at corner edges, or applied along a wall between corner edges, or can be used singly or in multiples for 75 central or other vertical reinforcement as well as transverse resistance to carton deformation. For most universal use, the tubular member is provided with a cross-section in the shape of a right isosceles triangle 80 so that it not only fits within corner edges of rectangular boxes, but also provides a surface of relatively large area forming the hypotenuse for use against a flat surface to be reinforced, such as a wall between the 85 corner edges of a container.

Two factors that affect the cubical rigidity, both axial and transverse, provided by reinforcement columns in a container are the surface area contact between the rein- 90

forcing members and the walls of the container, and the distance that such contact extends from the corners. The greater the distance from the corner, the greater the 5 moment of deformation resistance. In particular, a binding force is created by an adhesive or other bond established between the container and the amount of wall surface of the reinforcing member in frictional or 10 adherent contact therewith that provides an integrated area factor affecting rigidity, and there is a moment arm factor due to the distance of the surface bonded from the corner as determined by the shape and dimensions 15 of the reinforcing member. A tubular corner support of right triangular configuration has the advantage of occupying a minimum of usable central carton space, in a container having planar sides, in relation to the 20 wall surface contact area and moment arm length established by mutual contact between the tubular member and the container walls. For example, a square cross section support with comparable corner contact sur-25 face occupies twice the usable carton area as a triangular cross section support, while cylindrical supports afford only line or tangential contact with the sides of a container. For a given central space sacrifice, the dis-30 tance of such a tangential contact of a cylindrical support from the apex of the container corner is shorter than that of a triangular member and its integrated frictional force opposing transversing carton deform-35 ation is much smaller.

A further characteristic of the present tubular construction support of right isosceles triangular cross section is the somewhat greater degree of axial resilience afford-40 ed by the larger area of the hypotenuse side, as compared with a tubular construction support of square or circular cross section. It is believed that this resiliency may relieve momentary impact stresses that other-45 wise would cause failure in a more brittle

construction.

Triangular or substantially triangular tubular supporting members embodying the present invention may be fabricated of axi-50 ally oriented materials with fibres predominantly oriented in one direction. The member may be a resin moulding incorporating glass fibre reinforcement. Preferably however, a sheet of fabric of axially oriented 55 material is rolled into a tubular shape, triangular in cross section, with the fibres of the material extending longitudinally and the layers are bonded together by means of an adhesive. High axial compressive or ten-60 sile resistance is obtained in the finished member from the inherent strength of the fibres in their lengthwise direction. Paper made by a cylinder machine, such as reprocessed kraft paper, has fibres predominantly 65 oriented in what is known as the "machine direction" of the paper, i.e., the direction in which the web of paper is produced from the cylinder of the paper making machine. The compressive strength of such webs is substantially greater, in the "machine direc- 70 tion" than the cross machine direction. This difference is advantageously employed to fabricate triangular tubular constructions by convolutely winding the paper shapes in a direction across the machine direction of 75 the paper. Such fibre orientation, coupled with the inherently good plybond characteristic of cylinder machine paper, results in a paper strength in the machine direction that may be two to four times greater than in 80 the cross direction. Other fibre-like materials having appropriate length-to-cross sectional strength characteristics may offer strength advantages when used to construct triangular or substantially triangular tubular 85 structures, but paper is advantageous because it has high strength, is relatively light, and is inexpensive.

A substantially triangular convex shape has the advantage over straight-sided struc- 90 tures of facilitating good adhesion and lamination while facilitating higher winding speeds by virtue of the slight wall curvature which tends to keep the sheet under tension during winding. At the same time, this 95 shape maintains a relatively long moment arm and appreciable area contact as compared with a tube of circular cross section.

Two examples of supporting members constructed in accordance with the inven- 100 tion, and their use, are illustrated in the accompanying drawings, in which:-

Figure 1 is a partial detailed perspective

view of one supporting member;

Figure 2 is a partial detailed perspective 105 view of another supporting member;

Figure 3 is a partial perspective view of the member of Figure 1 positioned in a corner of a container;

Figure 4 is a partial plan view on an en- 110 larged scale of the member and container of Figure 3;

Figure 5 is a partial perspective view of the member of Figure 2 positioned in the corner of a container;

Figure 6 is a partial plan view on an enlarged scale of the member and container of Figure 5; and,

Figure 7 is a plan view of a container reinforced with supporting members.

Figure 1 shows an elongated tubular member 10 of generally triangular cross section and including two flat side portions 12, 14 of equal dimensions in perpendicular planes, a third side portion or hypotenuse 16 con- 125 necting the side portions 12 and 14, and curved integral corner portions 18, 20, 22 at the junctures of the three side portions. In cross section, then, the member 10 is in the shape of a right-isosceles triangle with 130

115

120

rounded corners. The rounded corner portions 18, 20, 22 avoid weakening the tubular member at the junctures of the flat sides, facilitate the forming of the member 10, 5 which may be accomplished by rapidly winding sheet of material about a triangular-shaped mandrel, and facilitate close contact and a good bond between the windings at the corners. To assure these ad-10 vantages, the corner portions 18, 20, 22 should preferably have a radius of curvature at least one-tenth the distance between the corner portions 20, 22, adjacent the longest side portion 16 when the member is 15 fabricated by winding paper or the like about a mandrel. By way of illustration, the radius of curvature of the corner portions 18, 20, 22 of a generally triangular-shaped tube convolutely wound of paper is at least 20 one quarter inch when the distance between the corner portions 20, 22 measured along the inner surface of the side portion 16 is two and one-half inches. By way of example only, a typical member convolutely wound 25 of kraft paper and suitable for use as a container support column may have two flat sides of 2 1/4 inches in length joined at a corner by a curved portion of 3/8 inch radius, a hypotenuse side with a flat sur-30 face about 3 1/4 inches in length joined at corners to the other sides by curved portions of 3/8 inch radius, a total length of 60 inches, and a wall thickness of 3/8 inch. The member 10 is composed of axially 35 oriented sheet material having fibres of high compressive strength predominantly aligned longitudinally of the finished tubular member. When the sheet is wound into tubular form about a mandrel, rounded mandrel 40 corners facilitate the attainment of better between-ply lamination and prevent creasing and weakening of the material, which could occur if the corners of the mandrel had sharp angles. As a result, it is possible to 45 use material of lower tensile strength and wind at higher speeds without weakening the material. For added strength, the fibre material layers are bonded together with adhesive and/or impregnated with a hard-50 ening material, such as an adhesive or resin. In the embodiment shown, the support member 10 is formed of paper, such as reprocessed kraft paper formed on cylinder machines. This is low in cost and has fibres 55 that extend predominantly in one direction, which corresponds to the longitudinal extent of the web of paper as formed and which is referred to as the "machine direction" of the paper. The paper is in a single 60 sheet, or a lamination of multiple plies, or more than a single sheet, coated with an air drying adhesive or chemically linking thermoplastic or thermosetting resin and is convolutely wound to provide a plurality of 65 layers, typically 8 to 11 layers in one pre-

ferred embodiment. The outer end of the sheet is shown at 26 and the inner end at 28. The paper is wound across the machine direction so that the fibres of the paper extend predominantly along the length of the 70 member. In the preferred embodiment at least the outer end of the sheet forming the member 10 is skived, i.e., tapered in thickness, and is quite flexible, allowing it to lie flat against the underlying layers until the 75 adhesive sets. This facilitates manufacture and permits the use of thicker paper which otherwise could not conveniently be used because the end of the sheet would spring up from the wound member. The thicker 80 paper facilitated by the skived end permits a strong tubular member to be wound with fewer windings, increasing the speed of production and reducing costs.

The member 10 as shown in Figure 1 85 may be manufactured by winding sheet material on an elongated mandrel. Most advantageously the member is wound initially to a triangular shape, which is more difficult than winding a cylinder, but which 90 provides a much stronger support than one which is shaped after winding. The sheet material to be wound is as wide as the desired length of the member 10 and is convolutely wound under tension upon the man- 95 drel. The inner end 28 is placed on the mandrel and the mandrel is rotated about its longitudinal axis. A number of layers are wound (depending upon the thickness and strength of the material and the ultimate strength desired in the finished product) and the outer end 26 is adhered in place. Alternatively, a continuous web can be used and cut when the member has the required thickness. However, in forming the preferred 105 embodiment from commercially available kraft paper manufactured on cylinder paper machines, a sheet of paper must be cut from the web or roll of paper, as supplied, to the length of the support desired. While this is 110 inconvenient, it permits winding the paper transversely to the machine direction, which is along the web, resulting in a tubular member having superior strength over a member wound directly from a web. The cut 115 sheet material is coated with an adhesive and then wound in the direction across the web. If the sheet material is pre-coated or already impregnated with an adhesive, the coating step is omitted.

A modified form of the generally triangular-shaped structure of Figure 1 is shown in Figure 2 and indicated generally by reference numeral 10'. The tubular structure 10' is generally triangular in cross section but 125 otherwise of identical construction to the member 10 and corresponding parts are identified with similar reference numerals with a prime designation. The structure is substantially triangular in that the side por- 130

120

tions 12', 14', 16' are slightly curved rather than straight, yet the structure is a threesided member of generally right-triangular configuraion constructed to fit within a cor-5 ner of a rectangular box. The slight convex curvature, as shown, facilitates convolutely winding the structure from sheet material at a rapid rate while constantly maintaining a tension on the material. It will be appreci-10 ated that a substantially triangular shape wih slightly concave sides can be formed by winding a triangular tube and post-forming it. Good corner bearing moments can be attained with such a shape, but fabri-15 cation is more complex.

With a structure having flat sides, the tension on the sheet material being wound is maintained by the pull exerted through contact at each corner of the winding man-20 drel or preceding layer since, theoretically at least there is no contact between the sheet material and the flat side until rotation brings the next adjacent corner into contact with the maerial, at which time that corner 25 then exerts a tension or pulling force due to its effective lever arm length from the

central axis of the winding mandrel. Thus, there is relatively little force urging adjacent layers into intimate contact along the 30 flat sides of the structure and the rate at which the rotating mandrel, conventionally driven at a constant angular speed, demands sheet material is extremely non-uniform making it difficult to maintain winding ten-

35 sion as material is placed on the flat sides. The slight convex curvature of the sides 12', 14', 16' causes the location that exerts tension on the sheet material as the structure is wound to progressively move from each 40 successive corner across a side of the struc-

ture to the next corner in a rolling action. This not only makes higher winding speeds and more uniform tension possible by creating a more uniform demand for sheet mate-45 rial during winding, it also assures that each

layer will be pressed against the preceding layer at all points about the periphery of the structure. At the same time, as long as the radius of curvature is maintained rela-

50 tively large, e.g., at least as great as the distance from corner portion to corner portion of the respective side portion, the area contact and distance of such contact from a corner of a container will remain relatively 55 large as will be described subsequently in

connection with Figures 2 and 6.

The tubular structures 10 and 10' are advantageously used to reinforce rectangular cardboard containers to increase the 60 cubical rigidity and to bear the compressive load when the containers are stacked. Figures 3 to 6 illustrate the manner in which these structures are secured in each corner of a container to provide large area contact 65 with the container wall and long moment

arms while occupying only a small part of the internal volume of the container.

A partial, corner portion, of a box-type container 35 is shown in Figures 3 and 4, for example a corrugated cardboard box or 70 carton. Two side walls 36, 38 are mutually perpendicular with a bottom 40 and top (not shown). The tubular member 10 of a length essentially equal to the height of the side walls 36, 38 is located at the juncture 75 of walls 36, 38 and abuts the bottom 40. Side portion 12 of the member 10 is against side wall 38 and side portion 14 is against side wall 36 and are adhered over the contacting area, as by a suitable adhesive indi- 80 cated at 41. Alternatively, staples or other fastening means can be used to attach the member to the side walls. The area of surface contact of both side portions 12, 14 extends along the entire height of the tubular 85 member and along the entire width of each side portion, as indicated at a in connection with side portion 14. The length of the moment arm that resists distortion of the mutually perpendicular relationship of the 90 container walls 36, 38 and bottom 40 is represented by d, which is the distance along the walls 36, 38 from their juncture to the farthest point of adherence between the respective wall and the reinforcing member 10. 95 The distances a and d are about equal in the member 10 and, except for the rounded corner portions 18, 20, 22, have been maximized by the substantially triangular cross sectional shape of the tubular member with respect to the volume occupied and the periphery of the member. Because the cubical rigidity is a direct function of the integrated moments of the resistance, which is the summation of the products of the distances on 105 the support from the carton wall intercepts and the adhesive strength per unit area, maximum transverse reinforcement is achieved with the substantially triangularshaped tubular member 10'.

The same box 35 is shown in Figures 5 and 6 with the substantially triangular-

shaped tubular member 10'.

The same box 35 is shown in Figures 5 and 6 with the substantially triangular- 115 shaped tubular member 10' located at the juncture of walls 36, 38. Because of the slight curvature of the side portions 12', 14'. the contact area between the member 10' and the container walls 36, 38 is somewhat 120 less than that between the walls and the member 10, as indicated by the shorter length of in Figures 5 and 6. A substantial area of mutual contact is created, notwithstanding the curved side portions 12', 14' 125 by distortion of the container wall portions that abut the member 10'. As compared with a flat-sided member 10, some area contact is lost adjacent the corner portions 18'. 20', 22' due to the curvature of the side por- 130

tions 12', 14', yet the contact area is adequate to assure a strong bond as with an adhesive 41'. The curvature of the side portions 12', 14' has a lesser effect upon the 5 effective moment arm length d' of the member 10' because the length of the moment arm is diminished only by the decreased contact adjacent the corner portions 20', 22' and not by the decreased contact adja-10 cent the juncture of the container walls 36. 38. As compared with a tubular member of cylindrical cross-sectional shape of similar perimeter or area, this substantially triangular construction 10' provides substantially 15 increased contact area and effective moment arm length, yet occupies less usable space in the container. At the same time, it facilitates rapid winding when fabricated from sheet material. Moreover, the effective 20 moment arms of the substantially triangular-shaped member can be increased either by effective cementing with a self-adhering filling adhesive, or by stapling or mechanically attaching the support to the container 25 wall at points beyond the closest contact of the curved side of the support, i.e. further away from the apex of the triangular member. It will be apparent that a substantially triangular-shaped member having slightly 30 concave sides will have somewhat less area contact with the container walls than a triangular member but will maintain a maximum moment arm length. Another manner in which tubular mem-

35 bers 10 can be used to reinforce a container is shown in Figure 7 in conjunction with a box with a base or bottom wall 46 and perpendicular side walls 44. Four members 10 are located at the inside corners formed by 40 the side walls 44 and four additional members are located one adjacent each wall 44 intermediate the corners. For optimum strength, the longest side wall 16 of each of the four additional members 10 bears 45 against the associated side wall of the box to maximise the area of mutual contact. In addition, the smallest dimension, i.e., the altitude or distance of the triangular-shaped cross section from the wall 16 to the corner 50 portion 18, extends inwardly and thus the usable space of the container occupied by the member is kept small. The four additional members can also afford protection to many objects inside the container by act-55 ing as a "stand-off" or cushioning spacer between the object and the carton wall.

WHAT WE CLAIM IS:-

1. An elongate stiff tubular supporting member having a unitary wall including at 60 least one layer of material extending jointlessly around its whole periphery, the wall being substantially triangular in cross section and incorporating elongate strengthgiving components aligned predominantly longitudinally of the member.

2. A member according to claim 1, which is formed of rolled sheet material incorporating fibres which extend predominantly axially of the member, and an adhesive bonding the layers of the sheet mate- 70

rial together.

3. A member according to claim 2, wherein the sheet material is reprocessed cylinder-machine kraft paper oriented with the machine direction of the paper extend- 75 ing parallel to the longitudinal axis of the member.

4. A member according to any one of the preceding claims, wherein the corners of the triangular cross section are rounded 80 and the distance between two adjacent corners is no more than ten times the radius of a corner.

5. A member according to any one of the preceding claims, in which a cross section of the member is substantially a right isosceles triangle.

6. A member according to any one of the preceding claims, the sides of which are curved transversely of their length.

7. A member according to claim 6, in which the sides are convex.

8. A member according to claim 1. substantially as described with reference to Figures 1, 3 and 4, or to Figures 2, 5 and 6, 95 of the accompanying drawings.

9. A box-like container having at least one corner edge reinforced by a member according to any one of the preceding claims, the member having two of its sides in inti- 100 mate contact with and secured to inside surfaces of the two container walls meeting at the corner edge.

10. A container according to claim 9, which has a further reinforcing member loca. 105 ted with one side against and secured to a wall of the container between but parallel to two corner edges.

11. A container according to claim 9, substantially as described with reference to 110

the accompanying drawings.

For the Applicants:—

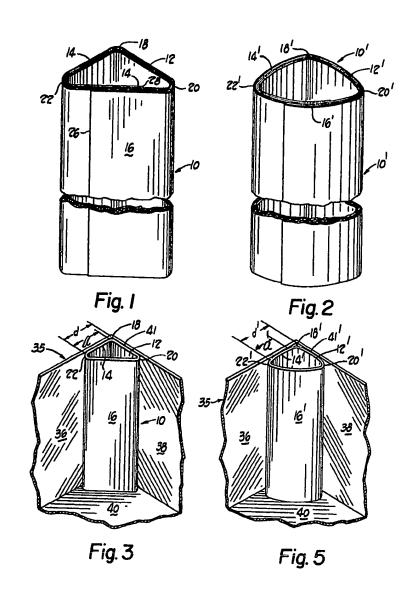
GILL, JENNINGS & EVERY,

Chartered Patent Agents,

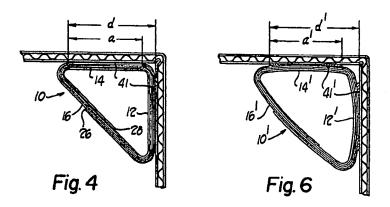
51/52 Chancery Lane, London, WS2A 1HN.

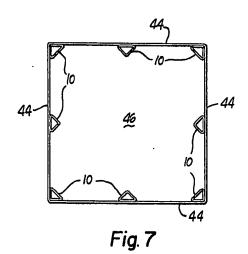
Printed for Her Majesty's Stationery Office by The Tweeddale Press Ltd., Berwick-upon-Tweed. 1971
Published at the Patent Office, 25 Southampton Buildings, London WC2A 1AY from which copies may be obtained.

1243716 COMPLETE SPECIFICATION
2 SHEETS
This drawing is a reproduction of the Original on a reduced scale
Sheet 1



1243716 COMPLETE SPECIFICATION 2 SHEETS This drawing is a reproduction of the Original on a reduced scale Sheet 2





This Page is Inserted by IFW Indexing and Scanning Operations and is not part of the Official Record

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:
☐ BLACK BORDERS
☐ IMAGE CUT OFF AT TOP, BOTTOM OR SIDES
X FADED TEXT OR DRAWING
BLURRED OR ILLEGIBLE TEXT OR DRAWING
☐ SKEWED/SLANTED IMAGES
☐ COLOR OR BLACK AND WHITE PHOTOGRAPHS
☐ GRAY SCALE DOCUMENTS
☐ LINES OR MARKS ON ORIGINAL DOCUMENT
☐ REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY
□ OTHER:

IMAGES ARE BEST AVAILABLE COPY.

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.